Soft elasticity and microstructure in smectic C elastomers

August 21, 2006

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Smectic C elastomers are layered materials exhibiting a solid-like elastic response along the layer normal and a rubbery one in the plane. The set of strains K_C minimizing the elastic energy contains a one-parameter family of simple stretches associated with an internal degree of freedom, coming from the in-plane component of the director. We investigate soft elasticity and the corresponding microstructure by determining the quasiconvex hull of the set K_C , and use this to propose experimental tests that should make the predicted soft response observable.

1 Introduction

Liquid crystal elastomers display a number of interesting mechanical and optical properties, with potential applications ranging from nonlinear optics to artificial muscles, due to the coupling between liquid crystal ordering transition and rubber elasticity [25]. Smectic C liquid crystals are characterized by rod-like molecules (mesogens) assembled in a layered structure, and tilted at a fixed angle with respect to the layer normal (see Figure 1). The mesogens are attached to polymer chains, which are cross-linked to obtain a rubber-like solid; the coupling to liquid crystal ordering leads to rubbery response in the tangential directions, and solid-like along the layer normal. Monodomain smectic C elastomers were recently synthesized [14] (see also discussion and references in [25, Chapter 12]); they exhibit spontaneous shear at the smectic A–smectic C phase transition [15]. Experimental interest in smectic C elastomers is also strongly motivated by the existence of a chiral ferroelectric phase.

A microscopic model based on statistical mechanics was recently derived in [2]. The model treats the polymers as Gaussian coils, with the cross-linkers

FIGURE 1: Sketch of the geometry of smectic C elastomers. The unit vector n gives the mesogen orientation in the deformed configuration, F is the deformation gradient, $F^{-T}w_0$ (or, equivalently, $\text{cof } Fw_0$) gives the normal to the smectic layers in the deformed configuration.

constrained to lie between the smectic layers. The free energy is obtained by taking a quenched average over the distribution of the chain endpoints at cross-linking. This leads to an elastic stored energy density expressed as a function of the local deformation gradient, see below.

In [2] soft modes were predicted, i.e., a nontrivial set K_C of energy-minimizing deformations was identified. Soft modes have also been predicted based on a phenomenologically derived Lagrangian elastic energy [23]. We show here that K_C is not quasiconvex, and hence that zero-energy microstructures can be formed. In particular, we find that the set of macroscopic strains which can be realized with zero energy is much larger than K_C . We characterize all such zero-energy macroscopic deformations by computing the quasiconvex hull of K_C . Our approach is based on the tools of the calculus of variations (see, e.g., [3, 9, 17, 12]), which have been remarkably successful, e.g., for shape-memory alloys [5] or nematic elastomers [25, Chapter 8].

The explicit computation of quasiconvex hulls in realistic three-dimensional physical systems is far from straightforward, even more so when working with finite deformations. Examples where this has been possible are nematic elastomers [11], and (at least partially) crystalline solids undergoing a cubic-to-tetragonal martensitic phase transition [13]. By computing the quasiconvex hull for smectic C elastomers and by exploiting this result to discuss the experimental accessibility of soft deformation paths we provide a further example in which the variational approach proves successful. The application

of these techniques to predict the result of stretching experiments on liquid crystal elastomers has been demonstrated in [6, 7, 8].

2 Statement of the problem and main results

The statistical mechanical model [2] gives the elastic stored energy density

$$W_C(F) = \begin{cases} \frac{1}{2}\mu \min_{n \in N(F)} \left[|F|^2 + \left(\frac{1}{\alpha^2} - 1 \right) |F^T n| - 3 \right] \\ \quad + \frac{1}{2}B \left(\frac{|U_0^{-1}w_0|}{|F^{-T}w_0|} - 1 \right)^2 & \text{if } \det F = \alpha, \\ +\infty & \text{else.} \end{cases} \quad (2.1)$$

Here $F \in \mathbb{R}^{3 \times 3}$ is the deformation gradient relative to a reference configuration chosen in order to fully exploit the cylindrical symmetry of the material (see Appendix), $U_0 = \text{Id} + (\alpha - 1)n_0 \otimes n_0$ is the deformation gradient at cross-linking, w_0 is a fixed unit vector chosen such that $U_0^{-1}w_0$ is orthogonal to the smectic layers at cross linking,

$$N^{(F)} = \left\{ n \in S^2 : n \cdot \frac{F^{-T}w_0}{|F^{-T}w_0|} = \cos \theta \right\},$$

and $n_0 \in N^{(U_0)}$ is the orientation of the mesogens at cross-linking. The quantities $\mu > 0$, $B > 0$, $\alpha > 1$, and $\theta \in (0, \pi/2)$ are material parameters. This expression differs from the one given in [2] by a change of variables in the reference configuration, see Appendix. The fact that the energy W_C is only finite on matrices with fixed determinant reflects the assumption of incompressibility by which all deformations from the initial configuration are volume-preserving. The choice of the value α is simply dictated by notational convenience. The parameter α is physically related to the anisotropy of the polymer chains and hence to the amplitude of the spontaneous deformations (see Section 3); θ characterizes the angle formed by the director with the layer normal (in particular, the case of smectic A elastomers is recovered for $\theta = 0$); and $B \gg \mu$ are the elastic moduli normal and tangential to the layer normal.

The function W_C defined in (2.1) is nonnegative, its minimum is zero, and is attained by matrices in the set

$$K_C = SO(3) \{ \text{Id} + (\alpha - 1)n \otimes n : n \cdot w_0 = \beta \} = SO(3) \bigcup_{n \in N_C} U_n, \quad (2.2)$$

where

$$U_n = \text{Id} + (\alpha - 1)n \otimes n$$

and

$$N_C = \{n : n \in S^2, n \cdot w_0 = \beta\} \quad (2.3)$$

(see Appendix for a proof of these simple facts). Here $\beta \in (0, 1)$ is a parameter related to the cosine of the angle θ between layer normal and director n , see (A.4).

A function $W : \mathbb{R}^{3 \times 3} \rightarrow \mathbb{R} \cup \{\infty\}$ is said to be quasiconvex if affine boundary conditions permit affine minimizers. Precisely, one requires that for all $F \in \mathbb{R}^{3 \times 3}$, and all open sets $\Omega \subset \mathbb{R}^3$, the energy of the affine map $x \mapsto Fx$ cannot be reduced without changing the boundary conditions, in the sense that

$$|\Omega| W(F) \leq \int_{\Omega} W(F + \nabla y) dx$$

for all $y \in W_0^{1,\infty}(\Omega; \mathbb{R}^3)$ for which the integral exists. Given a compact set $K \subset \mathbb{R}^{3 \times 3}$, one defines its quasiconvex hull as the set of points which cannot be separated from K by quasiconvex functions, i.e.,

$$K^{\text{qc}} = \left\{ F \in \mathbb{R}^{3 \times 3} : W(F) \leq \inf_{F' \in K} W(F') \right. \\ \left. \text{for all } W : \mathbb{R}^{3 \times 3} \rightarrow \mathbb{R} \text{ quasiconvex.} \right\}.$$

Physically, the set K^{qc} consists of the macroscopic deformation gradients which can be realized with zero energy. Indeed, it can be shown that K^{qc} is the set of matrices $F \in \mathbb{R}^{3 \times 3}$ such that there is a bounded sequence $y_j \in W^{1,\infty}(\Omega; \mathbb{R}^3)$ such that $y_j(x) = Fx$ on $\partial\Omega$ for all j , and $\text{dist}(\nabla y_j, K) \rightarrow 0$ in measure (this is true for any open and bounded set $\Omega \subset \mathbb{R}^3$ with $|\partial\Omega| = 0$). For a more detailed presentation of these concepts see, e.g., [9, 17, 12].

The following theorem gives an explicit formula for K_C^{qc} .

Theorem 2.1. *Let K_C be as in (2.2), with $\beta \in (0, 1)$, $\alpha > 1$, and w_0 a unit vector. Then,*

$$K_C^{\text{qc}} = \left\{ F \in \mathbb{R}^{3 \times 3} : \det F = \alpha, \quad \lambda_1(F) \geq 1, \right. \\ \left. |Fw_0|^2 \leq 1 + (\alpha^2 - 1)\beta^2, \quad |\text{cof } Fw_0|^2 \leq \alpha^2 - (\alpha^2 - 1)\beta^2 \right\}. \quad (2.4)$$

Here and below $\lambda_1(F) \leq \lambda_2(F) \leq \lambda_3(F)$ denote the ordered singular values of F , i.e., the ordered eigenvalues of $(F^T F)^{1/2}$.

Remark 2.2. *In the case $\alpha \in (0, 1)$ one obtains*

$$K_C^{\text{qc}} = \left\{ F \in \mathbb{R}^{3 \times 3} : \det F = \alpha, \quad \lambda_3(F) \leq 1, \right. \\ \left. |Fw_0|^2 \leq 1 + (\alpha^2 - 1)\beta^2, \quad |\text{cof } Fw_0|^2 \leq \alpha^2 - (\alpha^2 - 1)\beta^2 \right\}.$$

In the following we focus on the physically-relevant case $\alpha > 1$.

For a comparison, recall that the zero level set of the energy for (ideally soft) nematic elastomers reads, with the present notations,

$$K_N = SO(3) \left\{ \text{Id} + (\alpha - 1)n \otimes n : n \in S^2 \right\} = SO(3) \bigcup_{n \in S^2} U_n.$$

Clearly, $K_C \subset K_N$; notice that K_N is five dimensional, while K_C is only four dimensional. This corresponds to the fact that K_N has full rotational symmetry, whereas K_C has only cylindrical symmetry. The quasiconvex hull of K_N is [11]

$$K_N^{\text{qc}} = \left\{ F \in \mathbb{R}^{3 \times 3} : \det F = \alpha, \quad \lambda_1(F) \geq 1 \right\}.$$

Clearly $K_C^{\text{qc}} \subset K_N^{\text{qc}}$, notice, however, that both sets are eight dimensional. In fact, even for the case of cubic-to-tetragonal phase transitions, where the corresponding set of energy-minimizing states K_{ct} is only three dimensional, the hull $K_{\text{ct}}^{\text{qc}}$ turns out to be eight dimensional [13]. The mechanical implication of this property is that, starting from a point in the relative interior of K^{qc} , any small-enough volume-preserving deformation is soft.

We now turn to a more precise characterization of the microstructures leading to the relaxation result above. First we show that, for all matrices F which are in the relative interior of K_C^{qc} , the variational problem

$$\text{minimize } \int_{\Omega} W_C(\nabla y) dx : \quad \text{among all } y \text{ such that } y(x) = Fx \text{ on } \partial\Omega$$

has a Lipschitz-continuous minimizer, which obeys $W_C(\nabla y) = 0$ almost everywhere. In the proof we use the convex integration result by Müller and Šverák [18]; for alternative approaches to the same problem, see [10, 16].

Proposition 2.3. *Under the same assumptions and in the notation of Theorem 2.1, let*

$$F_* \in (K_C^{\text{qc}})^{\text{int}} = \left\{ F \in \mathbb{R}^{3 \times 3} : \det F = \alpha, \quad \lambda_1(F) > 1, \right. \\ \left. |Fw_0|^2 < 1 + (\alpha^2 - 1)\beta^2, \quad |\text{cof } Fw_0|^2 < \alpha^2 - (\alpha^2 - 1)\beta^2 \right\}. \quad (2.5)$$

Then, for any open domain $\Omega \subset \mathbb{R}^3$, the partial differential inclusion

$$\begin{cases} \nabla y \in K_C & \text{a.e. in } \Omega \\ y(x) = F_*x & \text{on } \partial\Omega \end{cases}$$

has a Lipschitz solution $y : \Omega \rightarrow \mathbb{R}^3$.

FIGURE 2: Schematic representation of the deformation in (2.6).

The Lipschitz maps y constructed by convex integration have very complex geometric structures. Simpler patterns emerge by studying minimizing sequences in the form of laminates (see Figure 2). For example, a first-order laminate is obtained by considering deformations y_ε whose gradients oscillate between two values, say A and B , with volume fractions λ and $1 - \lambda$. The matrices A and B have to satisfy the condition $A - B = a \otimes \nu$, for some vectors $a \in \mathbb{R}^3$ and $\nu \in S^2$. The deformations have the form

$$y_\varepsilon(x) = Cx + a\varepsilon\chi\left(\frac{x \cdot \nu}{\varepsilon}\right), \quad (2.6)$$

where $C = \lambda A + (1 - \lambda)B$ is the average of the laminate, and χ is a 1-periodic function such that

$$\chi(t) = \begin{cases} (1 - \lambda)t & \text{if } 0 \leq t \leq \lambda \\ \lambda(1 - t) & \text{if } \lambda \leq t \leq 1. \end{cases}$$

As $\varepsilon \rightarrow 0$, the deformation y_ε approaches uniformly the affine map Cx . Laminates of higher order are obtained by iterating this construction, see [9, 17, 12]. The laminates relevant for Theorem 2.1 are described in the following proposition.

Proposition 2.4. *Under the same assumptions and in the notation of Theorem 2.1,*

- (i) *All matrices in K_C^{qc} are averages of third-order laminates supported on K_C .*
- (ii) *All matrices in K_C^{qc} where at least one of the three inequalities is an equality can be obtained as averages of second-order laminates supported on K_C .*
- (iii) *All matrices in K_C^{qc} where two of the three inequalities are equalities, and only those, can be obtained as averages of first-order laminates supported on K_C .*

All proofs are given in Section 4.

3 Physical and experimental implications

Spontaneous deformations consisting of reversible shears of up to $\sim 20^\circ$ have been measured in smectic C elastomers [15], but no further mechanical experimental data is available. In comparison, smectic A elastomers have been studied in much greater detail: samples with the smectic layer compression modulus (B in (2.4)) taking very large values [20, 19], or small values [21, 22] have been fabricated and mechanically tested. We propose here experimental geometries where soft elastic response and microstructure formation are expected for smectic C elastomers. We focus on a thin-film geometry since monodomain samples have only been obtained as thin films.

A mechanical experiment in which a specimen experiences a sequence of macroscopically affine deformations corresponds to a path through the space of matrices; in practice, one always starts from the cross-linking configuration, which lies on the boundary of K_C^{qc} . Thus, the path can either move away from K_C^{qc} , or can first move into K_C^{qc} and eventually leave it later. In the ideal case, moving within K_C^{qc} requires zero energy and therefore no stress. In practice, due to various sources of non-ideality in the rubber (e.g., a preferred direction from the two-stage crosslinking process), the stress cannot be exactly zero. One expects the signature of K_C^{qc} to be a region which can be traversed with very small stress. For example, experiments on nematic elastomers have shown first a small, but rapid, increase in the stress, then a wide plateau with a much lower apparent elastic modulus, and finally a rapid increase in the stress after the plateau [25, Chapter 7.4].

In order to discuss experimental tests it is more convenient to work in a coordinate system in which the reference configuration is the one at cross

FIGURE 3: An illustration of the proposed experimental geometry, and of the coordinate system used. The relevant case has tension along z (i.e., $\gamma_z > 1$), and compression along x (i.e., $\gamma_x < 1$).

linking, which amounts to inverting the coordinate change discussed in the Appendix. Substituting $\Lambda = FU_0^{-1}$ into expression (2.4) shows that $F \in K_C^{\text{qc}}$ corresponds to $\Lambda \in K_*^{\text{qc}} = K_C^{\text{qc}}U_0^{-1}$. Equivalently, K_*^{qc} is the set of matrices $\Lambda \in \mathbb{R}^{3 \times 3}$ satisfying the following relations:

$$\det \Lambda = 1, \quad (3.1)$$

$$\lambda_1(\Lambda U_0) \geq 1, \quad (3.2)$$

$$|\Lambda U_0^2 k_0|^2 \leq 1 + (r^2 - 1) \cos^2 \theta, \quad (3.3)$$

$$|\Lambda^{-T} k_0|^2 \leq 1. \quad (3.4)$$

Here $r = \alpha^2$, θ is defined by

$$\cos^2 \theta = \frac{\beta^2}{\alpha^2 + (1 - \alpha^2)\beta^2}$$

and $k_0 = U_0^{-1}w_0/|U_0^{-1}w_0|$.

The experimental configuration considered here is a thin film in the (e_1, e_3) plane, layer normal $k_0 = e_3$, and director tilted in the e_1 direction, i.e., $n_0 = \sin \theta e_1 + \cos \theta e_3$ (see Fig. 3).

Shearing tests

Consider deformations of the form

$$\Lambda_S(\gamma) = \begin{pmatrix} 1 & 0 & \gamma \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix},$$

which correspond to the geometry in which spontaneous shear was observed [15] when cooling from the smectic A to smectic C phase, because θ evolves from 0 to its current value. This matrix satisfies (3.4) and (3.2) with equality for $\gamma \leq 0$. The remaining inequality (3.3) then reduces to the following

$$(1 + (r - 1) \cos^2 \theta)^2 + (\gamma + (r - 1) \cos \theta (\gamma \cos \theta + \sin \theta))^2 \leq 1 + (r^2 - 1) \cos^2 \theta$$

We conclude that $\Lambda_S(\gamma) \in K_*^{\text{qc}}$ provided that

$$\gamma_* \leq \gamma \leq 0, \quad \text{where} \quad \gamma_* = -\frac{(r - 1) \sin 2\theta}{\sin^2 \theta + r \cos^2 \theta}.$$

In this case, the accompanying microstructure can also be determined explicitly. In particular, it is a simple laminate between $\Lambda_S(0) = \text{Id}$ and $\Lambda_S(\gamma_*)$ with varying volume fractions, and with lamination planes parallel to the smectic layers, i.e., in the notation of (2.6), $B = \text{Id}$, $A = \Lambda_S(\gamma_*)$, $C = \Lambda(\gamma)$, and $\nu = k_0$, and $\lambda = \gamma/\gamma_*$. Therefore the nematic director initially has the value n_0 everywhere, and with increasing γ it takes the value n_1 (corresponding to $\Lambda_S(\gamma_*)$) on larger and larger portions of the sample.

Notice that the matrices

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ \gamma & 0 & 1 \end{pmatrix}, \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & \gamma & 1 \end{pmatrix}, \begin{pmatrix} 1 & 0 & 0 \\ \gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}, \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & \gamma \\ 0 & 0 & 1 \end{pmatrix}, \begin{pmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

do not give rise to soft deformations for $\gamma \neq 0$. The first two matrices do not satisfy (3.4), the third and fourth do not satisfy (3.3), and the fifth does not satisfy (3.2).

Simple shear testing of the sample may prove impractical to carry out experimentally as the sample may buckle for large imposed shears. Attributing any observed plateau in the stress-strain curve to soft deformation path may then be difficult. We now consider an experimental geometry in which the sample is under tension.

Tensile tests

Consider applying a biaxial extension to the film, with the direction of the largest stretch at an angle ϕ to the layer normal. This could be done, for example, by cutting out a small rectangular piece of elastomer from an existing film at the required angle to the layer normal and then applying biaxial stretches parallel to the sample edges (x and z axes, see Fig. 3). We denote the rotated axes by (e_x, e_y, e_z) , to distinguish them from the original axes (e_1, e_2, e_3) . In practice we expect that the results here should also apply to

uniaxial extension along the e_z axis (and not only to the prescribed biaxial extension), as the other two directions should adjust so that the deformation remains in K_*^{qc} . The deformation gradient for extension along e_z is of the form

$$\Lambda_T(\gamma_x, \gamma_y, \gamma_z) = \begin{pmatrix} \gamma_x \cos^2 \phi + \gamma_z \sin^2 \phi & 0 & (\gamma_x - \gamma_z) \cos \phi \sin \phi \\ 0 & \gamma_y & 0 \\ (\gamma_x - \gamma_z) \cos \phi \sin \phi & 0 & \gamma_z \cos^2 \phi + \gamma_x \sin^2 \phi \end{pmatrix}$$

where γ_x , γ_y and γ_z are the principal stretches. We now calculate the range of values of ϕ for which paths of this form lie within K_*^{qc} . Due to the symmetry of Λ_T , it is only necessary to consider $0 \leq \phi \leq \pi/2$.

Clearly by using (3.1) we obtain $\gamma_y = 1/(\gamma_x \gamma_z)$, hence we drop it from the notation. The remaining inequalities defining K_C^{qc} show that $\Lambda_T \in K_*^{\text{qc}}$ if the following conditions hold:

$$\frac{\sin^2 \phi}{\gamma_x^2} + \frac{\cos^2 \phi}{\gamma_z^2} \leq 1, \quad (3.5)$$

$$0 \leq 1 + \gamma_z^2 \gamma_x^2 r - \gamma_x^2 (\cos^2(\phi + \theta) + r \sin^2(\phi + \theta)) - \gamma_z^2 (\sin^2(\phi + \theta) + r \cos^2(\phi + \theta)), \quad (3.6)$$

$$\gamma_x \gamma_z \leq 1, \quad (3.7)$$

$$1 + (r^2 - 1) \cos^2 \theta \geq \gamma_z^2 \left(\frac{r+1}{2} \cos \phi + \frac{r-1}{2} \cos(\phi + 2\theta) \right)^2 + \gamma_x^2 \left(\frac{r+1}{2} \sin \phi + \frac{r-1}{2} \sin(\phi + 2\theta) \right)^2. \quad (3.8)$$

Here (3.5) arises from the condition (3.4), (3.6) and (3.7) arise from (3.2), and (3.8) arises from (3.3). An illustration of the set of pairs (γ_x, γ_z) satisfying these four inequalities is given in Fig. 4. All four conditions are equalities for $\Lambda_T(1, 1) = \text{Id}$, corresponding to the fact that this matrix is on the boundary of K_*^{qc} .

We now check if, for suitable choices of the angle ϕ , there are curves in the (γ_x, γ_z) plane which stay within K_*^{qc} . To do this, we compute the slopes of the four curves given above, and compare their values at the point $(1, 1)$. It turns out that there is a nonempty set which satisfies all four conditions only if

$$\frac{\pi}{4} - \theta + \frac{1}{2} \arctan \frac{\tan \theta}{r} \leq \phi \leq \frac{\pi}{4}.$$

Therefore soft elasticity is expected only for samples with orientation in this particular range.

FIGURE 4: Illustration of the stretches γ_x, γ_z for which the deformation Λ_T is soft (i.e., in K_*^{qc}), for $r = 2$ and $\theta = 22.5^\circ$. (a) stretching direction $\phi = 36^\circ$, (b) stretching direction $\phi = 39^\circ$.

We are now interested in the amount of soft deformation that can be sustained by the sample. Precisely, for any value of ϕ we compute the maximal soft stretch in the z direction,

$$\gamma_z^{\max} = \max \{ \gamma_z : \Lambda_T(\gamma_x, \gamma_z) \in K_*^{\text{qc}} \text{ for some } \gamma_x \} .$$

Computing $\gamma_z^{\max}$ involves solving several algebraic equations, corresponding to the various pairs of inequalities in (3.5)-(3.8). The results are reported in Figure 5 for some realistic values of the parameters.

4 Proofs of the results in Section 2

We start by recalling a result on the relaxation of the two-well problem [4, 24]. Its proof is given at the end of this section for the convenience of the reader.

Lemma 4.1. *For any pair $n_1, n_2 \in S^2$, the hull of the two wells*

$$K_{12} = SO(3)U_{n_1} \cup SO(3)U_{n_2}$$

is given by

$$\begin{aligned} K_{12}^{\text{qc}} = \{ & F \in \mathbb{R}^{3 \times 3} : \det F = \alpha, \quad \alpha Fv = \text{cof } Fv, \\ & |Ff_1| \leq |U_{n_1}f_1|, \quad |Ff_2| \leq |U_{n_1}f_2| \} . \end{aligned} \quad (4.1)$$

FIGURE 5: An illustration of the expected amplitude of the soft plateau $\gamma_z^{\max}$ as a function of orientation angle ϕ (in degrees). Full (black) curve, $r = 2$ and $\theta = 22.5^\circ$; dotted (blue) curve, $r = 2.5$ and $\theta = 22.5^\circ$; short-dashed (red) curve, $r = 2$ and $\theta = 30^\circ$; long-dashed (green) curve, $r = 2$ and $\theta = 15^\circ$.

Here

$$v = \frac{n_1 \wedge n_2}{|n_1 \wedge n_2|}, \quad f_1 = \frac{n_1 + n_2}{|n_1 + n_2|}, \quad f_2 = \frac{n_1 - n_2}{|n_1 - n_2|}. \quad (4.2)$$

The set K_{12}^{qc} is polyconvex; each matrix in K_{12}^{qc} is the average of a second-order laminate supported on K_{12} ; the set of matrices which are averages of first-order laminates supported on K_{12} is the subset of K_{12}^{qc} where one of the two inequalities is an equality.

Geometrically, v is the normal to the plane spanned by n_1 and n_2 ; the vectors (v, f_1, f_2) form an orthonormal basis, and the f_i are (up to a sign) the only two unit vectors orthogonal to v which fulfill $|U_{n_1} f| = |U_{n_2} f|$. Further, since $\det F = \alpha$ the condition $\alpha Fv = \text{cof } Fv$ is equivalent to $F^T Fv = v$. This implies, in particular, that one of the singular values of F is 1.

Proof of Theorem 2.1. Let $\tilde{K}$ be the set in the right-hand side of (2.4), i.e., the set of matrices $F \in \mathbb{R}^{3 \times 3}$ such that

$$\det F = \alpha, \quad (4.3)$$

$$|Fw_0|^2 \leq 1 + (\alpha^2 - 1)\beta^2, \quad (4.4)$$

$$|\text{cof } Fw_0|^2 \leq \alpha^2 - (\alpha^2 - 1)\beta^2, \quad (4.5)$$

$$\lambda_1(F) \geq 1. \quad (4.6)$$

The set $\tilde{K}$ is clearly polyconvex, as it is defined as the intersection of sublevel sets of polyconvex functions (recall that $\lambda_1(F) = \det F / \lambda_3(\operatorname{cof} F)$, hence (4.6) can be equivalently replaced by $\lambda_3(\operatorname{cof} F) \leq \alpha$). Therefore it suffices to show that any matrix in $\tilde{K}$ is the average of a laminate supported on K . Due to the rotational invariance, it further suffices to consider symmetric matrices in $\tilde{K}$.

We decompose $\tilde{K}$ into three sets $\tilde{K}^{(i)}$, $i = 1, 2, 3$. In the first one all three inequalities are equalities,

$$\begin{aligned} \tilde{K}^{(1)} := \left\{ F \in \tilde{K} : \lambda_1(F) = 1, \quad |Fw_0|^2 = 1 + (\alpha^2 - 1)\beta^2, \right. \\ \left. |\operatorname{cof} Fw_0|^2 = \alpha^2 - (\alpha^2 - 1)\beta^2 \right\}. \end{aligned}$$

The second one contains matrices with one singular value equal to 1,

$$\tilde{K}^{(2)} := \left\{ F \in \tilde{K} : \lambda_1(F) = 1 \right\}$$

The third one contains matrices with all singular values strictly larger than 1,

$$\tilde{K}^{(3)} := \left\{ F \in \tilde{K} : \lambda_1(F) > 1 \right\}.$$

We claim that

- (i) $\tilde{K}^{(1)} = K_C$;
- (ii) all matrices in $\tilde{K}^{(2)}$ are averages of second-order laminates supported on two wells in K_C ;
- (iii) all matrices in $\tilde{K}^{(3)}$ are averages of simple laminates supported in $\tilde{K}^{(2)}$.

Since $\tilde{K} = \tilde{K}^{(2)} \cup \tilde{K}^{(3)}$, this will imply the thesis. It remains to prove the three claims. For notational simplicity, in the following we work with $w_0 = e_3$.

Proof of Claim (iii). Let $F \in \tilde{K}^{(3)}$, and consider the rank-one line

$$F_t = F (\operatorname{Id} + te_1 \otimes e_2).$$

To prove the claim it suffices to determine two values of t , say $t_+ > 0 > t_-$, such that F can be written as an average of F_{t_+} and F_{t_-} , with $F_{t_\pm} \in \tilde{K}^{(2)}$. To do this, we first compute

$$\operatorname{cof} F_t = \operatorname{cof} F (\operatorname{Id} - te_2 \otimes e_1), \quad \text{and} \quad \det F_t = \alpha.$$

Therefore the quantities $\det F_t$, $|F_t e_3|$, and $|\operatorname{cof} F_t e_3|$ do not depend on t . Consider now the function

$$f(t) = \lambda_1(F_t).$$

This is continuous, $f(0) > 1$, and $\lim_{t \rightarrow \pm\infty} f(t) = 0$. To see the latter, it suffices to observe that

$$\infty = \lim_{t \rightarrow \pm\infty} |F_t|^2 = \lim_{t \rightarrow \pm\infty} \lambda_3^2(F_t) + \lambda_2^2(F_t) + \lambda_1^2(F_t) \leq \lim_{t \rightarrow \pm\infty} \frac{3\alpha^2}{\lambda_1^4(F_t)},$$

since $\det F_t = \alpha$ implies $\lambda_3(F_t) = \alpha/\lambda_2(F_t)\lambda_1(F_t) \leq \alpha/\lambda_1^2(F_t)$. We conclude that the equation $f(t) = 1$ has at least one positive and one negative solution (actually they are unique, since λ_1 is concave along volume-preserving rank-one directions). The solutions are the desired t_+ and t_- .

Proof of Claim (ii) We can assume without loss of generality that F is symmetric, so that $\lambda_1(F) = 1$ means that F has an eigenvalue 1. Let v be the corresponding eigenvector. Exploiting the cylindrical symmetry we can assume that $v \cdot e_2 = 0$, and obtain

$$Fv = v \quad \text{for} \quad v = \begin{pmatrix} \cos \phi \\ 0 \\ \sin \phi \end{pmatrix}. \quad (4.7)$$

We intend to determine values of n_1 and $n_2 \in N_C$ such that we can use Lemma 4.1, with this vector v . It is convenient to start from the two vectors f_i , as in (4.2). Indeed, f_1 is a unit vector normal to both w_0 and v , hence $f_1 = e_2$; in turn, f_2 is normal to both f_1 and v . In components, we obtain

$$f_1 = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \quad \text{and} \quad f_2 = \begin{pmatrix} -\sin \phi \\ 0 \\ \cos \phi \end{pmatrix}.$$

We now claim that $F \in \tilde{K}$ implies

$$|Ff_1|^2 \leq 1 + (\alpha^2 - 1) \left(1 - \frac{\beta^2}{\cos^2 \phi} \right) \quad (4.8)$$

and

$$|Ff_2|^2 \leq 1 + (\alpha^2 - 1) \frac{\beta^2}{\cos^2 \phi}. \quad (4.9)$$

Since $1 \leq \lambda_1(F) \leq |Ff_1|$, (4.8) implies that $\beta^2 \leq \cos^2 \phi$. We can therefore define

$$n_{1,2} = \begin{pmatrix} -\beta \tan \phi \\ \pm \sqrt{1 - \beta^2 / \cos^2 \phi} \\ \beta \end{pmatrix} \in K_C.$$

These vectors have been determined so that (4.2) is satisfied. In turn, the expressions on the right-hand side of (4.8) and (4.9) are exactly the values

of $|U_{n_1}F_i|^2 = |U_{n_2}F_i|^2$. Therefore by Lemma 4.1 (4.8) and (4.9) imply that F is in the second lamination convex hull of $SO(3)\{U_{n_1}, U_{n_2}\} \subset K_C$.

It remains to prove the claimed (4.8)-(4.9). To do so, we write

$$w_0 = \sin \phi v + \cos \phi f_2,$$

and observe that $\{v\}, \{v\}^\perp$ are eigenspaces of F . Therefore,

$$|Fw_0|^2 = \sin^2 \phi |Fv|^2 + \cos^2 \phi |Ff_2|^2,$$

and using (4.7) and (4.4) we get (4.9). Analogously,

$$|\operatorname{cof} Fw_0|^2 = \sin^2 \phi |\operatorname{cof} Fv|^2 + \cos^2 \phi |\operatorname{cof} Ff_2|^2.$$

Using (4.7) and (4.5) we get

$$|\operatorname{cof} Ff_2|^2 \leq \alpha^2 - (\alpha^2 - 1) \frac{\beta^2}{\cos^2 \phi}. \quad (4.10)$$

We recall that if $F^T Fv = v$, then

$$|F\mu| = |\operatorname{cof} F(v \wedge \mu)| \quad \text{for all } \mu \in \mathbb{R}^3, \quad \mu \cdot v = 0. \quad (4.11)$$

To see this, it suffices to verify it for symmetric F , so that v is an eigenvector with eigenvalue 1. Then, $\operatorname{cof} F(v \wedge \mu) = Fv \wedge F\mu = v \wedge F\mu$, and the two vectors are orthogonal. Using (4.11) in (4.10), we obtain (4.8).

Proof of Claim (i) If $F \in K_C$, then $F = QU_n$ for some $n \in N_C$, hence

$$|Fw_0|^2 = |U_n w_0|^2 = 1 + (\alpha^2 - 1)(n \cdot w_0)^2 = 1 + (\alpha^2 - 1)\beta^2$$

and

$$|\operatorname{cof} Fw_0|^2 = |\alpha U_n^{-1} w_0|^2 = \alpha^2 + (1 - \alpha^2)(n \cdot w_0)^2 = \alpha^2 + (1 - \alpha^2)\beta^2,$$

therefore $F \in \tilde{K}^{(1)}$.

If $F \in \tilde{K}^{(1)} \subset \tilde{K}^{(2)}$, then we can repeat the argument given in the proof of Claim (ii), and obtain that equality holds in (4.8) and (4.9). Since (v, f_1, f_2) is an orthonormal basis,

$$|F|^2 = |Fv|^2 + |Ff_1|^2 + |Ff_2|^2 = 2 + \alpha^2.$$

Recalling that $\det F = \alpha$ and $\lambda_1(F) = 1$, we have

$$\lambda_2(F)\lambda_3(F) = \alpha, \quad \lambda_2^2(F) + \lambda_3^2(F) = 1 + \alpha^2,$$

hence $\lambda_2(F) = 1, \lambda_3(F) = \alpha$. Therefore $F = QU_n$, for some $n \in S^2$. Finally,

$$|Fw_0|^2 = |U_n w_0|^2 = 1 + (\alpha^2 - 1)(n \cdot w_0)^2,$$

therefore $(n \cdot w_0)^2 = \beta^2$. Replacing if necessary n with $-n$, we conclude that $n \cdot w_0 = \beta$, hence $n \in N_C$ and $F \in K_C$. $\square$

Proof of Remark 2.2. The proof follows the same steps as the one of Theorem 2.1, replacing the condition $\lambda_1 \geq 1$ with the condition $\lambda_3 \leq 1$. In particular, to show that $\beta^2 \leq \cos^2 \phi$ (after (4.8)), one uses (4.9) and the fact that $\lambda_3 \leq 1$. $\square$

Proof of Proposition 2.4. Part (i) follows from the claims (ii) and (iii) in the proof of Theorem 2.1.

We now prove part (iii). First-order laminates only involve two values of the director n , hence by Lemma 4.1 their average satisfies $\lambda_1(F) = 1$, and one of the two inequalities in (4.1) is an equality. Therefore also one of the other two inequalities in (2.4) is an equality, see proof of Claim (i) above.

Conversely, assume that $\lambda_1(F) = 1$, and that one of the other inequalities in (2.4) is an equality. Then, arguing as in the proof of Theorem 2.1, we obtain that either (4.8) or (4.9) is an equality. Therefore, application of Lemma 4.1 as in the proof of Claim (ii) above gives a first-order laminate with average F .

Finally, assume that

$$|Fw_0|^2 = 1 + (\alpha^2 - 1)\beta^2 \quad \text{and} \quad |\operatorname{cof} Fw_0|^2 = \alpha^2 - (\alpha^2 - 1)\beta^2,$$

and consider the construction used in the proof of Claim (iii). The matrices F_t constructed there belong to $\tilde{K}^{(1)} = K_C$.

It remains to show part (ii) of Proposition 2.4. If $\lambda_1(F) = 1$, then $F \in \tilde{K}^{(2)}$, hence it is the average of a second-order laminate by Claim (ii). If instead one of the other inequalities is an equality, we consider a first-order laminate as in the proof of Claim (iii) above. For the resulting matrices two inequalities are equalities, hence by Part (iii) (proven above) are the average of first-order laminates. This concludes the proof. $\square$

Proof of Proposition 2.3. Proposition 2.3 is proven on the basis of the convex integration result by Müller and Šverák [18, Theorem 1.3], by constructing a suitable in-approximation for the set K_C (see (4.14) below for a definition). This will be done by considering a family of variants of the set K_C which interpolates between $SO(3)$ and the original set K_C . To do this, it is necessary to work with constant determinant, and it is convenient to make the dependence on α and β explicit in the notation. We change variables according to

$$\tilde{F} = \alpha^{-1/3} F,$$

and write

$$\tilde{K}_{\alpha,\beta} = SO(3) \left\{ \alpha^{-1/3} \operatorname{Id} + (\alpha^{2/3} - \alpha^{-1/3}) n \otimes n : n \in N_C^\beta \right\},$$

where N_C^β is defined as in (2.3). The hull can be characterized as

$$\tilde{K}_{\alpha,\beta}^{\text{qc}} = \{F \in \mathbb{R}^{3 \times 3} : \det F = 1, \psi_j(F) \leq \phi_j(\alpha, \beta), j = 1, 2, 3\} \quad (4.12)$$

where

$$\begin{aligned} \psi_1(F) &= \frac{1}{\lambda_1(F)}, & \phi_1(\alpha, \beta) &= \alpha^{1/3}, \\ \psi_2(F) &= |Fw_0|^2, & \phi_2(\alpha, \beta) &= \alpha^{-2/3} + (\alpha^{4/3} - \alpha^{-2/3})\beta^2, \\ \psi_3(F) &= |\text{cof } Fw_0|^2, & \phi_3(\alpha, \beta) &= \alpha^{2/3} - (\alpha^{2/3} - \alpha^{-4/3})\beta^2. \end{aligned}$$

By Claim (i) in the proof of Theorem 2.1, replacing inequalities with equalities this reduces to $\tilde{K}_{\alpha,\beta}$, i.e.,

$$\tilde{K}_{\alpha,\beta} = \{F \in \mathbb{R}^{3 \times 3} : \det F = 1, \psi_j(F) = \phi_j(\alpha, \beta) \ j = 1, 2, 3\}. \quad (4.13)$$

We want to construct an in-approximation, i.e., a sequence of uniformly bounded, relatively open sets $U_i \subset \{F \in \mathbb{R}^{3 \times 3} : \det F = 1\}$ such that

$$U_i \subset (U_{i+1})^{\text{rc}}, \quad \text{and} \quad U_i \rightarrow \tilde{K}. \quad (4.14)$$

Here $U_i \rightarrow \tilde{K}$ means that $F_i \rightarrow F$, $F_i \in U_i$ implies $F \in \tilde{K}$; U^{rc} denotes the rank-one convex hull of U , see [9, 17, 12]. We claim that we can choose $\alpha_i > 1$, $\beta_i \in (0, 1)$, $\varepsilon_i > 0$ such that

$$U_i = \left\{F : \det F = 1, \text{dist}(F, \tilde{K}_{\alpha_i, \beta_i}) < \varepsilon_i\right\}$$

satisfies (4.14). These sets are relatively open, uniformly bounded, and the convergence to $\tilde{K}$ is ensured provided that

$$\alpha_i \rightarrow \alpha, \quad \beta_i \rightarrow \beta, \quad \text{and} \quad \varepsilon_i \rightarrow 0.$$

We shall choose α_i and β_i so that

$$\tilde{K}_{\alpha_i, \beta_i} \subset \left(\tilde{K}_{\alpha_{i+1}, \beta_{i+1}}^{\text{rc}}\right)^{\text{int}}. \quad (4.15)$$

Here A^{int} denotes the relative interior of the set $A \subset \{F : \det F = 1\}$. Since the first set in (4.15) is compact and the second relatively open, if (4.15) holds then we can choose $\varepsilon_i > 0$ such that (4.14) holds.

It remains to choose α_i and β_i so that (4.15) holds. Since by Proposition 2.4 $\tilde{K}_{\alpha_{i+1}, \beta_{i+1}}^{\text{rc}} = \tilde{K}_{\alpha_{i+1}, \beta_{i+1}}^{\text{qc}}$, recalling (4.12) and (4.13), (4.15) is equivalent to the condition

$$\phi_j(\alpha_i, \beta_i) < \phi_j(\alpha_{i+1}, \beta_{i+1}) \quad j = 1, 2, 3.$$

We claim that there is a curve γ starting from the point (α, β) and such that the three functions $\phi_j \circ \gamma$ are strictly decreasing along γ . If this is the case, it suffices to choose appropriately the points along γ to obtain sets fulfilling (4.15). Precisely, assume

$$\gamma(0) = (\alpha, \beta), \quad \nabla \phi_j \circ \gamma \cdot \gamma'(t) < 0 \text{ for } t \in [0, t_0], t_0 > 0. \quad (4.16)$$

(here (α, β) denote the values entering the statement, i.e., the parameters in (2.5)). Choose $t_1 \in (0, t_0)$ such that $\psi_j(F_*) < \phi_j(\gamma(t_0))$ for all j , which is possible since by assumption $\phi_j(F_*) < \phi_j(\gamma(0))$ for all j . Then, the points

$$(\alpha_i, \beta_i) = \gamma(2^{-i}t_1)$$

satisfy all requirements.

It remains to show existence of the curve γ with the properties given in (4.16). We prove this by showing existence of a vector field along which all $\nabla \phi_j$ are negative. For each (α, β) , the set of directions which have a negative component along $\nabla \phi_2$ is an open half-plane. The same holds for $\nabla \phi_3$. Since the two gradients do not sum to zero, the two half-planes intersect in a cone, and there is a direction on which both ϕ_2 and ϕ_3 are decreasing. We claim that in this direction also ϕ_1 is decreasing. Indeed,

$$\nabla \phi_2 + \alpha^{2/3} \nabla \phi_3 = \begin{pmatrix} \frac{2}{3}(1 + \beta^2)\alpha^{-5/3}(\alpha^2 - 1) \\ 0 \end{pmatrix}.$$

Therefore

$$\nabla \phi_1 = \frac{\alpha}{2(\alpha^2 - 1)(\beta^2 + 1)} [\nabla \phi_2 + \alpha^{2/3} \nabla \phi_3].$$

Since the fraction is positive, we conclude that if ϕ_2 and ϕ_3 are decreasing, so is ϕ_1 . $\square$

Proof of Lemma 4.1. Let $\tilde{K}$ denote the right-hand side of (4.1). This set is clearly polyconvex. Further, $K_{12} \subset \tilde{K}$. Even more, we claim that K_{12} equals the set of matrices in $\tilde{K}$ where both inequalities are equalities. To see this, assume

$$\det F = \alpha, \quad \alpha Fv = \operatorname{cof} Fv, \quad |Ff_1| = |U_{n_1}f_1|, \quad |Ff_2| = |U_{n_1}f_2|.$$

This implies

$$|F|^2 = |U_{n_1}|^2 = 2 + \alpha^2.$$

Therefore the singular values of F are $(1, 1, \alpha)$, i.e., $F = QU_n$, for some $n \in S^2$. Clearly $v \cdot n = 0$. Further,

$$(n \cdot f_i)^2 = (n_1 \cdot f_i)^2 = (n_2 \cdot f_i)^2 \quad i = 1, 2.$$

Therefore $n \in \{\pm n_1, \pm n_2\}$ and $F \in K_{12}$.

Let now $F \in \tilde{K}$ be such that

$$|Ff_1| = |U_{n_1}f_1|, \quad |Ff_2| < |U_{n_1}f_2|.$$

the other case being equivalent. We consider the rank-one line

$$F_t = F(\text{Id} + tf_1 \otimes f_2).$$

We notice that $\det F_t$, F_tv , $\text{cof } F_tv$ and F_tf_1 do not depend on t . At the same time, $f(t) = |F_tf_2|$ is continuous, and diverges as $t \rightarrow \pm\infty$, hence there are two values $t_- < 0 < t_+$ such that $f(t_\pm) = |U_{n_1}f_2|$. For the matrices $F_{t_\pm}$ all inequalities are equalities, hence by the previous argument they are in K_{12} , and F is the average of a first-order laminate supported on them.

Finally, for a generic $F \in \tilde{K}$ we consider the rank-one line

$$F_t = F(\text{Id} + tf_2 \otimes f_1).$$

Reasoning as above, we can find two values of t such that

$$|F_{t_\pm}f_1| = |U_{n_1}f_1|,$$

and reduce to the previous case. The conclusion follows. $\square$

5 Discussion and outlook

In summary, we have determined the quasiconvex hull of the zero set of the energy density for smectic C elastomers derived in [2], and have shown that it contains a full-dimensional set of volume-preserving zero-energy deformations. We used our result to predict microstructure formation and soft elastic response in stretching experiments on thin sheets (see Fig. 5), and to propose experimental geometries that should make the effect visible.

In the related case of smectic A elastomers, which corresponds to taking $\beta = 1$, one obtains as zero set of the energy $K_A = SO(3)U_{w_0}$ (see [1]). Therefore the quasiconvex hull is trivial, $K_A^{\text{qc}} = K_A$. The mechanical interpretation of this fact is that there are no zero-energy soft modes. Microstructure formation and softening at intermediate stretches have, however, been observed experimentally [19] for stretches along the layer normal, and explained theoretically [1] as due to buckling of the smectic layers. Similar and more complex effects can be expected in smectic C.

The analysis in [1] can be recast in the present variational framework, leading to a partial determination of the quasiconvex envelope of the smectic

A energy density. This shows that there exists a large variety of physically-relevant regimes outside of the zero-energy set, and that the knowledge of the full quasiconvex envelope of the energy density may shed further light on the complex physics of these interesting materials. The determination of the envelope for the smectic A energy density is, in the general case, open, and even more so for smectic C.

Acknowledgements

This work was partially supported by Deutsche Forschungsgemeinschaft through the Schwerpunktprogramm 1095 *Analysis, Modeling and Simulation of Multiscale Problems* and by the Istituto Nazionale di Alta Matematica through the research project *Mathematical Challenges in Nanomechanics*.

A Appendix

In [2], the following energy density is derived from a statistical mechanical model

$$W_1(\Lambda) = \begin{cases} \frac{1}{2}\mu \min_{n \in N_1^{(\Lambda)}} [\text{Tr}(\Lambda U_0^2 \Lambda^T U_n^{-2}) - 3] \\ \quad + \frac{1}{2}B \left(\frac{1}{|\Lambda^{-T}k_0|} - 1 \right)^2 & \text{if } \det \Lambda = 1 \\ \infty & \text{else,} \end{cases}$$

where $\Lambda \in \mathbb{R}^{3 \times 3}$ is the deformation gradient with respect to the cross-linking configuration, k_0 is the unit normal to the smectic layers at cross-linking, and the smectic director n is a unit vector in the set

$$N_1^{(\Lambda)} = \left\{ n \in S^2 : n \cdot \frac{\Lambda^{-T}k_0}{|\Lambda^{-T}k_0|} = \cos \theta \right\}.$$

Further,

$$U_n = \text{Id} + (\alpha - 1)n \otimes n$$

is a uniaxial stretch along n , and $U_0 = U_{n_0}$, $n_0 \in N_1^{(\text{Id})}$ being the director at cross-linking. The expressions in [2] are written in terms of $r = \alpha^2$ and $\ell_n = U_n^2$.

As in the case of nematic elastomers, it is convenient to change reference configuration, in order to fully exploit the symmetry of the problem. In particular, we replace the variable Λ with F , defined by

$$F = \Lambda U_0 = \Lambda(\text{Id} + (\alpha - 1)n_0 \otimes n_0),$$

and correspondingly

$$\begin{aligned}
W_C(F) &= W_1(FU_0^{-1}) \\
&= \begin{cases} \frac{1}{2}\mu \min_{n \in N_2^{(F)}} \left[|F|^2 + \left(\frac{1}{\alpha^2} - 1 \right) |F^T n| - 3 \right] \\ \quad + \frac{1}{2}B \left(\frac{|U_0^{-1}w_0|}{|F^{-T}w_0|} - 1 \right)^2 & \text{if } \det F = \alpha, \\ \infty & \text{else.} \end{cases} \quad (\text{A.1})
\end{aligned}$$

Here

$$w_0 = \frac{U_0 k_0}{|U_0 k_0|},$$

and

$$N^{(F)} = N_1^{(FU_0^{-1})} = \left\{ n \in S^2 : n \cdot \frac{F^{-T}w_0}{|F^{-T}w_0|} = \cos \theta \right\}.$$

Notice that $|U_0 k_0| = 1/|U_0^{-1}w_0|$. Further, the director at cross-linking is the fixed vector $n_0 \in N_1^{(\text{Id})} = N^{(U_0)}$.

It remains to show that the function W_C defined in (A.1) is nonnegative, its minimum is zero, and is attained by matrices in the set defined in (2.2), namely,

$$K_C = SO(3) \{ \text{Id} + (\alpha - 1)n \otimes n : n \cdot w_0 = \beta \}. \quad (\text{A.2})$$

To see this, we observe that the square bracket in (A.1) satisfies

$$|F|^2 + \left(\frac{1}{\alpha^2} - 1 \right) |F^T n| - 3 \geq \lambda_1^2(F) + \lambda_2^2(F) + \frac{1}{\alpha^2} \lambda_3^2(F) - 3, \quad (\text{A.3})$$

where λ_i are the ordered singular values of F , with equality holding if $|F^T n| = \lambda_3(F)$. Since $\lambda_1 \lambda_2 \lambda_3 = \det F = \alpha$, the right-hand side of (A.3) is minimized when $\lambda_1 = \lambda_2 = \lambda_3/\alpha = 1$, its minimum is zero, and the minimizers are the matrices of the form

$$F = QU_m$$

where $m \in S^2$, and $Q \in SO(3)$. The left-hand side of (A.3), in turn, is minimized when additionally to the said conditions, n can be chosen so that (A.3) becomes an equality. This is equivalent to provided that $n = Qm \in N^{(F)}$, i.e.,

$$Qm \cdot \frac{F^{-T}w_0}{|F^{-T}w_0|} = \cos \theta.$$

The second term in (A.1) is also nonnegative, hence $W_C \geq 0$. We now check that the minimum of W_C is zero, and that it is attained by the matrices

of the form given in (A.2). To do this, it suffices to show that

$$K_C = \left\{ F : F = QU_m, \quad |F^{-T}w_0| = |U_0^{-1}w_0|, \quad Qm \cdot \frac{F^{-T}w_0}{|F^{-T}w_0|} = \cos \theta \right\},$$

where as above $m \in S^2$, $Q \in SO(3)$. Equivalently, we have to show that

$$K_C = \left\{ F : F = QU_m, \quad |U_m^{-1}w_0| = |U_0^{-1}w_0|, \quad U_m^{-1}m \cdot w_0 = |U_0^{-1}w_0| \cos \theta \right\},$$

The second condition is of the form $m \cdot w_0 = \beta$, with

$$\beta = |U_0^{-1}w_0| \alpha \cos \theta. \tag{A.4}$$

In particular, it is fulfilled by $m = n_0$. Since $|U_m^{-1}w_0|$ depends only on the scalar product $m \cdot w_0$, it is constant on the set K_C , hence equality is proven.

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